

The Role of the Rheology in Extrusion Processing & its impact upon Product Texture

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Rheology & Texture Influence of Rheology on Extrusion

The Rheology of an Extrusion Melt considers both the Viscous Effects and also the Elastic Effects associated with the Melt Flow.

The Rheology has a direct influence on the Product Characteristics via:

Control of the Bubble Growth Rate

Control of the Degree of Expansion

Control of the Degree of Curvature



The Rheology has a direct influence on the Process Design via:

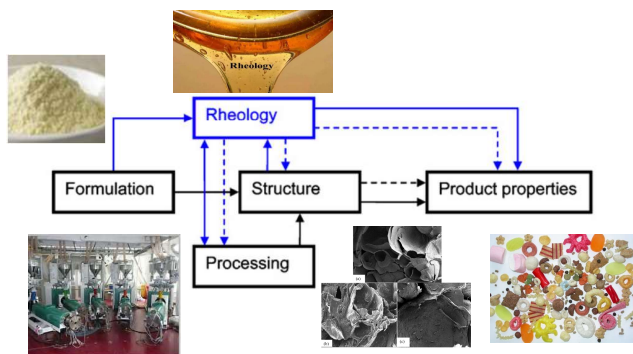
Control of the Die Pressure Drop

Control of the Screw Flow Dynamics

Control of the Screw Energy Consumption



Rheology & Texture



Extrusion is a highly interactive Process and the Formulation Rheology plays a pivotal role.

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Viscous Behaviour

“All things flow under the influence of a Force or Stress.”

The perceived differences between the numerous types of fluids that may be encountered relates to the Fluid Rheology and is measured via the Response Time of the given fluid to the imposed stress.

This is called the Relaxation Time.



Water in a Glass



High DE Glucose Syrup



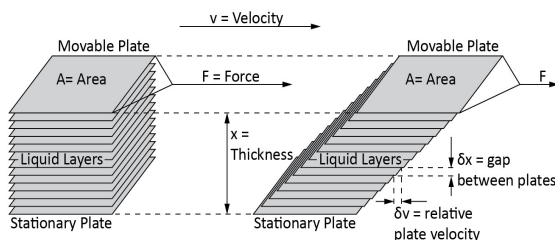
Nylon Thread being Drawn



Silly Putty Spilling

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A Thought Experiment - Fluid Flow



Whilst Fluids are a Continuum, they may be considered as existing as discrete “Layers”. The Frictional Interactions between these Layers may be considered as resulting in the observed Rheological Properties of the Fluid.

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Parameter Definitions

Shear Stress = Force / Area

$$\tau = F / A$$

Shear Rate = Velocity Differential / Gap

$$\dot{\gamma} = \delta v / \delta x \approx (v_{\max} - v_{\min}) / x$$

In an Extruder system the most important Shear Rates are:

The Flight Gap Shear Rate,

The Channel Shear Rate,

$$\dot{\gamma}_{\text{gap}} \approx \pi D_s N / g$$

[results in “Cooking”]

$$\dot{\gamma}_{\text{channel}} \approx \pi D_s N / H$$

[results in “Mixing”]

The Die Shear Rate,

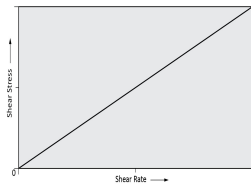
$$\dot{\gamma}_{\text{die}} \approx 8 v_D / D_d = 4 Q_{\text{net}} / \pi R^3$$

[results in “Skin Formation”]

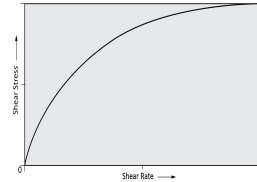


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Newtonian Fluid Behaviour



Non-Newtonian Fluid Behaviour



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A Definition for Fluid Viscosity

$$\text{Viscosity} = \text{Shear Stress} / \text{Shear Rate}$$

$$\mu = \tau / \gamma$$

For Newtonian Fluids (at a given Temperature)

$$\mu = \text{constant}$$

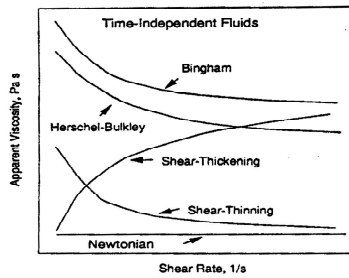
For Non-Newtonian Fluids (at a given Temperature), the Viscosity is not constant, thus

$$\mu_{\text{apparent}} \neq \text{constant, it is Shear Rate Dependent}$$

Note: For a Non-Newtonian Fluid we must refer to the Apparent Viscosity (at a specified Shear Rate).

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General Behaviour of Time-independent Fluids



Yield Stress in a Panna Cotta



Pseudoplastic Fluids



Bingham Plastic Fluids



Dilatant Fluids

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Some typical values of Fluid Viscosity for various Materials

Material	Viscosity
Water	1-5 cps
Blood	10 cps
Corn Syrup	50-100 cps
Maple Syrup	150-200 cps
Castor Oil	250-500 cps
Honey	2-3,000 cps
Molasses	5-10,000 cps
Chocolate Syrup	10-25,000 cps
Ketchup	50-70,000 cps
Peanut Butter	150-200,000 cps
Crisco/Lard	1-2,000,000 cps
Silicone Sealant	5-10,000,000 cps
Window Putty	100,000,000 cps

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The Herschel-Bulkley Model

$$\tau = \tau_y + m \gamma^n$$

and

$$\mu_{\text{apparent}} = \left[\tau_y / \gamma \right] + \left[m \gamma^{n-1} \right]$$

where,

τ_y = The Yield Stress

m = The Consistency Index

n = The Flow Behaviour Index

μ_{apparent} = The Apparent Viscosity

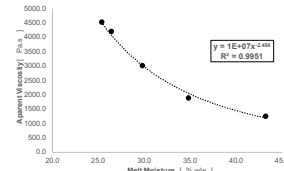
For most Food Extrusion Melts, $0.3 < n < 0.5$



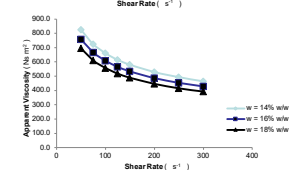
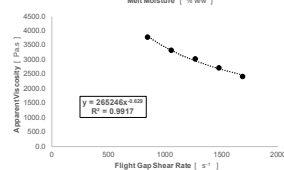
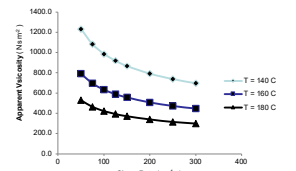
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Effect of w_M , γ_{gap} & T_M on Apparent Viscosity

Whole Wheat Flour



Maize Grits

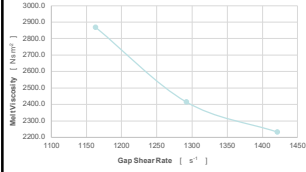


Note: This Data was obtained using Single Ingredients at Laboratory Scale [$D \approx 10 \text{ kg hr}^{-1}$]

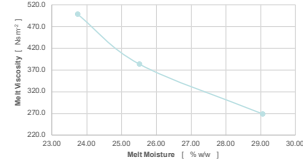
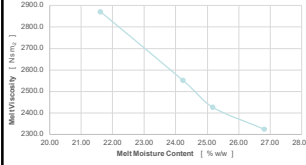
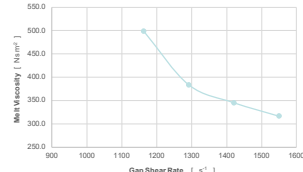
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Effect of w_M & γ_{gap} on Apparent Viscosity

Cocoa Shells



Rice Crispies



Note: This Data was obtained using Formulated Products at Industrial Scale [D = 600 kg hr⁻¹]

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The use of Cooking Viscometers

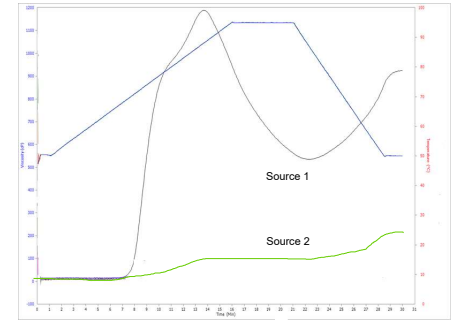
Soy Protein Isolates – Two different SPI Sources



Pertin Instruments RVA



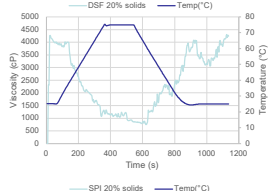
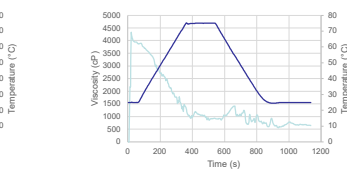
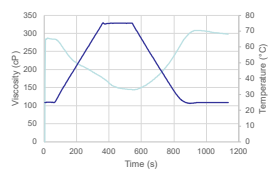
Brabender Micro Visco –Amylograph



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The use of Cooking Viscometers

Soya-based Products – Recipe Blending



RVA Pasting Profiles for a number of Soya-based Materials.
[All Samples tested using “non-standard” Test Parameters.]

Formulation Blend

DSF = 40%, SPC = 24%, SPI = 36%

What will the Pasting Curve Parameters be?

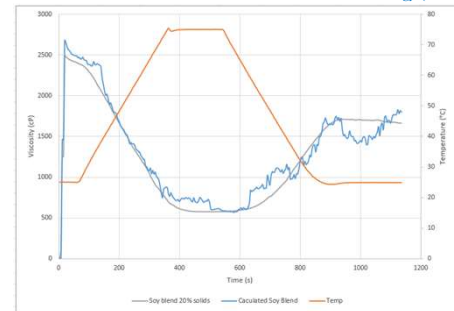
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Use of Cooking Viscometers

Soya-based Products – Recipe Blending

These Soya-based Materials were then Blended and the Mixture was subsequently Tested (using “non-standard” Test Parameters).

[The Test Data for the Raw Materials was used to estimate the Blend Rheology (see Grey Curve).]



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Effect of Temperature, Moisture and Fat on the Melt Viscosity

In general, for Non-Newtonian Fluids

$$\mu_{\text{apparent}} = m_0 e^{[a1/T]} e^{[a2w]} e^{[a3f]} \gamma^{n-1}$$

For an Extruder the Die Pressure Drop is related to the Melt Viscosity thus,

$$\Delta P \propto \mu_{\text{app}}$$

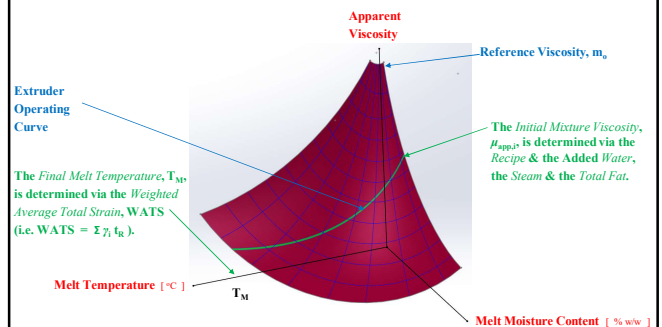
so,

$$\Delta P \propto e^{[a1/T]} e^{[a2w]} e^{[a3f]}$$

(if all else is constant)

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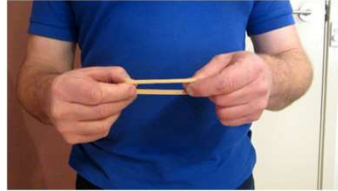
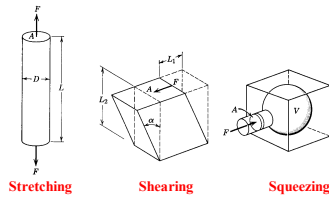
Extruder Operating Curve – Melt Rheology



$$\mu_{\text{apparent}} = m_0 e^{[a1/T]} e^{[a2w]} e^{[a3f]} \gamma^{n-1}$$

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Elastic Behaviour



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Visco-Elastic Behaviour



Memory Foam™



Selection of Extruded Products exhibiting Elastic Effects



“The Golden Rules of Extrusion Technology”

Golden Rule # 1

Extrusion System Flow Components

$$Q_{\text{drag}} - Q_{\text{pressure}} - Q_{\text{leakage}} = Q_{\text{net}} = K \Delta P / \mu_{\text{apparent}}$$

Screw Characteristic

Die Characteristic

where,

$$Q_{\text{net}} = \text{Total Melt Flow} / \text{Melt Density}$$

$$Q_{\text{drag}} = f[N, \text{Screw Geometry}, \text{Recipe}, \text{COF}_{\text{barrel}}]$$

$$Q_{\text{pressure}} = f[\Delta P, H^3, 1 / \mu_{\text{apparent}}]$$

$$Q_{\text{leakage}} = f[\Delta P, \text{Flight Gap}, 1 / \mu_{\text{apparent}}]$$

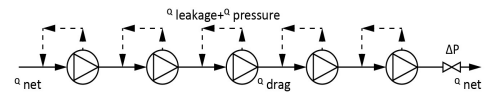
$$K = f[A, L, S, \text{COF}_{\text{die}}]$$

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Extruder Behavior Explained -

An Analogy for Extruder Operation

The operation of an extruder may therefore be considered as being equivalent to that of a *Multi-stage Pump with Slip*.



The Pump (or Extruder) will utilize as many Stages (or Screw Elements) as needed to deliver the Required Volumetric Output, Q_{net} , against the Operating Pressure, ΔP .



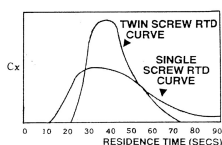
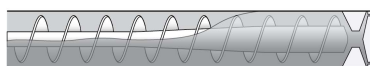
The Filled Length of an Extruder

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The Filled Length of the Extruder

The Filled Length (or the Choke Point) of the Extruder determines the magnitude of the Mean Residence Time, t_R .

The magnitude of t_R for the TSE is typically slightly lower than that for a SSE.



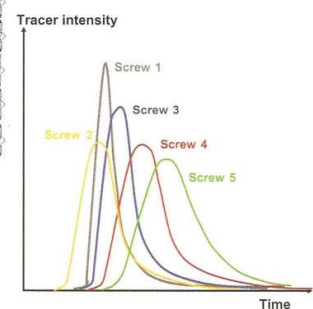
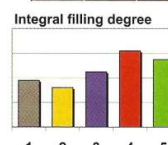
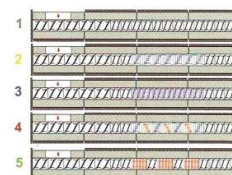
L_{fill}



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The Filled Length of the Extruder

The Residence Time Distribution (or RTD), however, is determined by the specific Screw Geometry.



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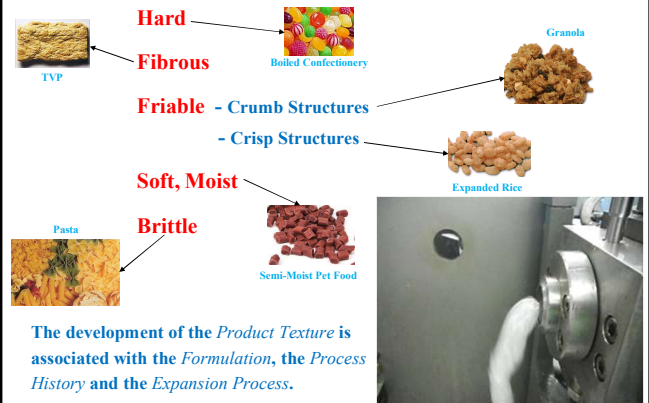
Estimation of the Apparent Viscosity of the Melt

The use of Extruder Operating Data

Dry Feed Rate, D	13.84	kg / hr
Water Flow Rate, W	6.13	kg / hr
Melt Flow Rate, M	19.97	kg / hr
Melt Density, ρ_M	1200	kg / m ³
Volume Flow, Q_{net}	4.623E-06	m ³ / s
$Q_{\text{net}} = M / \rho_M$		
Die Diameter, d	1.50	mm
Die Land Length, L	3.00	mm
Radius, R	7.500E-04	m
$k = \pi R^4 / 8 L$		
Die Conductance, k	4.142E-11	m ³ per Hole
Number of Die Holes	6	
Total Conductance, K	2.485E-10	m ³
Die Pressure, ΔP	2600	kPa
$\mu_{\text{app}} = K \Delta P / Q_{\text{net}}$		
Apparent Melt Viscosity, μ_{app}	139.77	Ns / m ²
	139770	cP

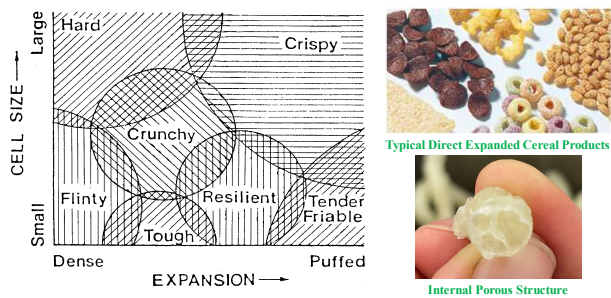
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Numerous types of *Product Textures* may be defined:



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Relationship between Structure and Expansion



The *Bubble Morphology* (i.e. *Bubble Size*, *Number of Bubbles* and the *Cell Wall Thickness*) is critical in determining the *Final Product Texture*.

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The Extrusion Cooking Process

If we consider any “Cooking Process” then we can say that

$$\text{Cook} = f(\text{Time, Temperature, Pressure \& Shear})$$

Pressure alone cannot “cook”, however, it does allow the Process to operate at an *Elevated Temperature* (i.e. $> 100^\circ\text{C}$), which significantly increases the *Rate of Cooking*, thereby reducing the *Cook Time*. In the simplest of terms we can therefore say that

$$\text{Formulation} + \text{Energy} \rightarrow \text{Product}$$

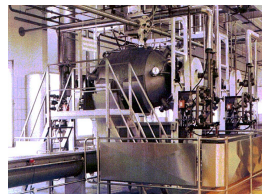
Clearly, it is the *Energy Input* that results in the *Transformation* (or *Cooking*) of the *Ingredients* within the *Formulation* into the *Product*.

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Product Cooking Systems



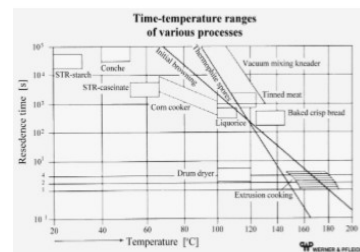
Batch Steam Pressure Cooker



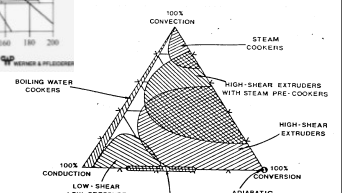
High Shear Extrusion Cooker

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Process Energy Inputs

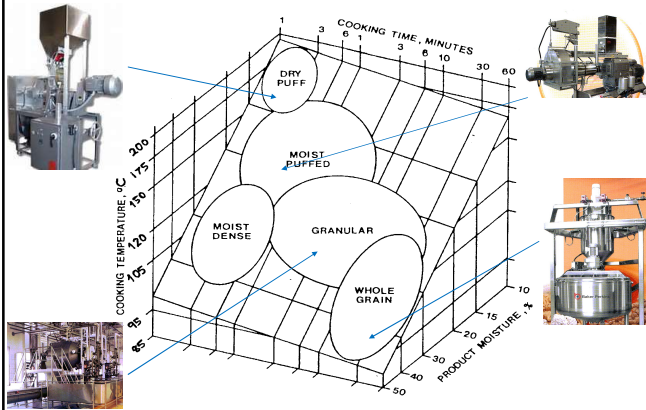


The *Processing Temperature*, the *Residence Time* and the *Energy Inputs* may be modified to change the *Product Characteristics*.



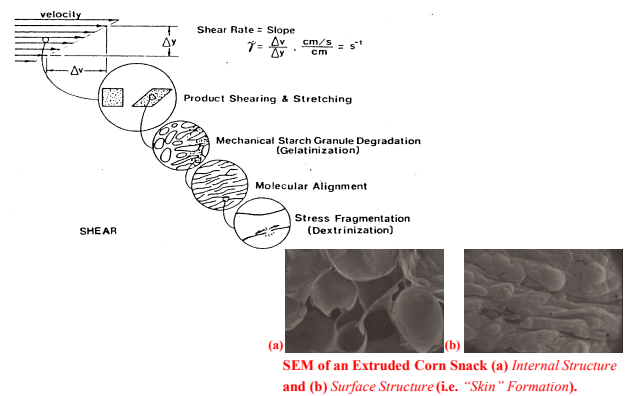
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Summary of Cooking Processes



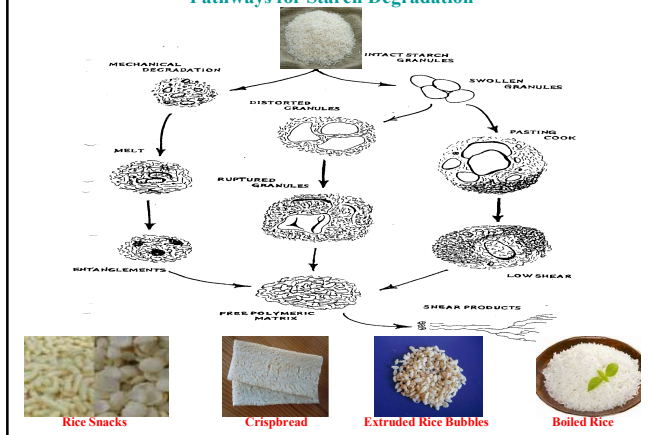
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The Role of Shear in the Extrusion Cooking Process



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Pathways for Starch Degradation



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The Role of Shear in the Extrusion Cooking Process

If we rearrange our definition for *Viscosity*, then we obtain the following expression

$$\tau = \mu_{\text{apparent}} \dot{\gamma}$$

Thus, for a given *Formulation*, at a given *Total Moisture Content* and *Temperature*, in the presence of a given *Shear Rate* (determined by the *Screw Geometry* and *Screw Speed*), an *Effective Shear Stress* is experienced within the *Fluid*, resulting in the *Degradation* (or "Cooking") of the *Ingredients*.

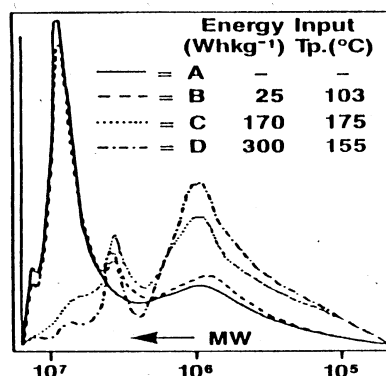
[Thus, in simplistic terms, it is the *Shear Stress* within the *Fluid* (which acts at the *Molecular Level*), that tells the *Ingredients* how to "break down", that is "how to cook"!]

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Influence of SME on the Mean Molecular Weight (MMW)

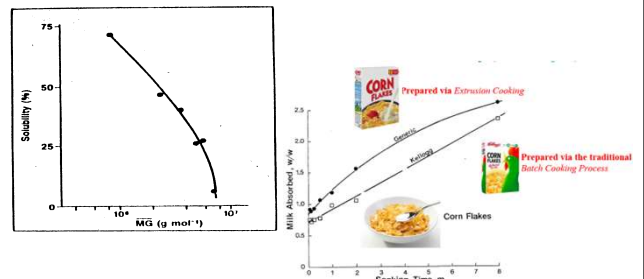
An increase in the SME leads to a significant increase in the Degree of Degradation of both the Starches (and also the Proteins).

$$\text{SME} = P_{\text{net}} / M$$



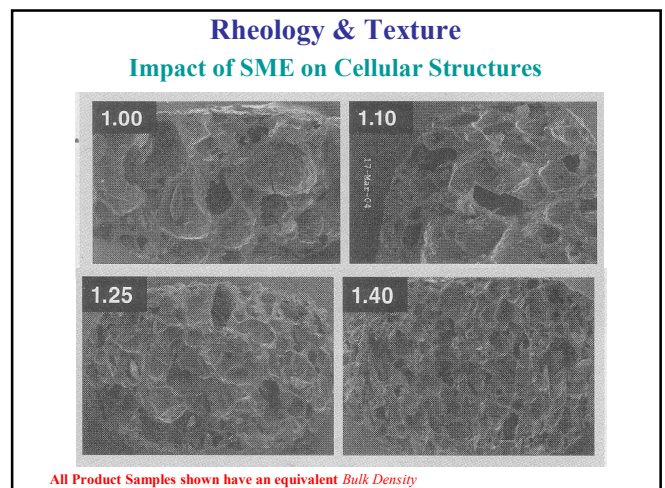
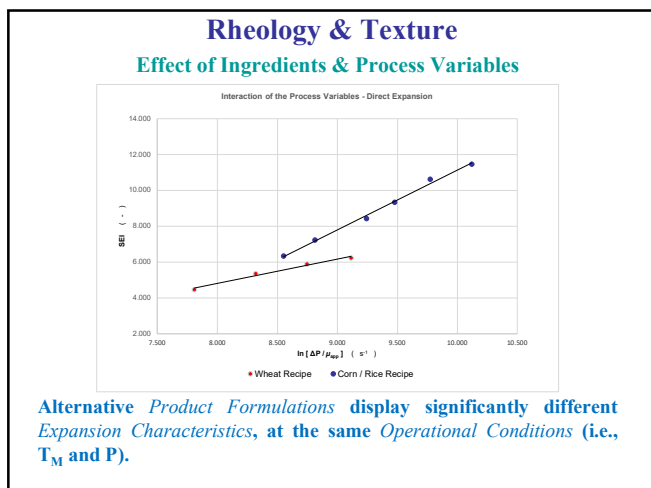
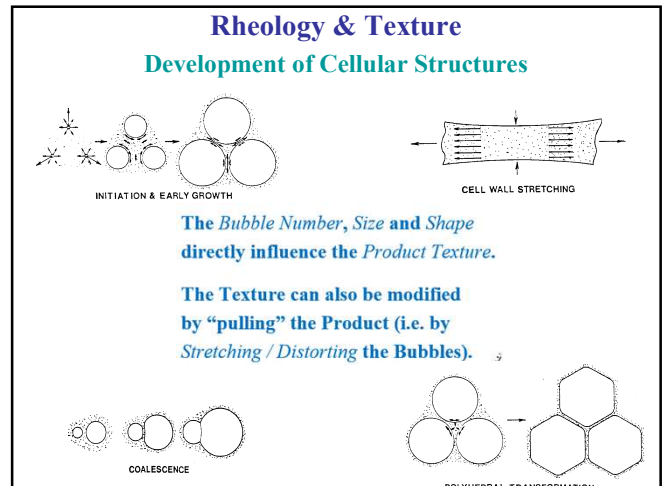
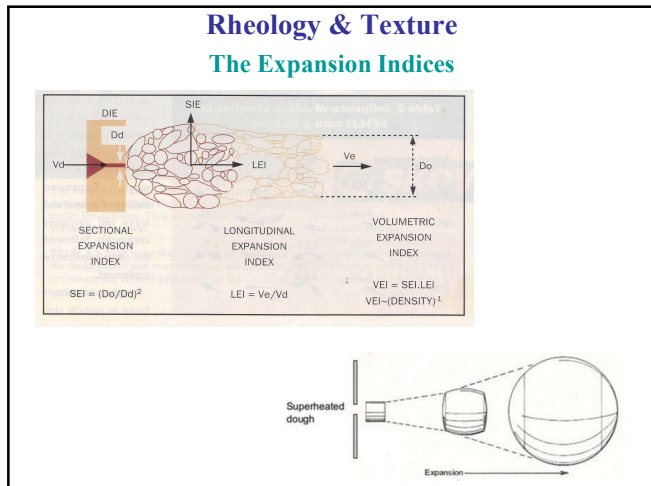
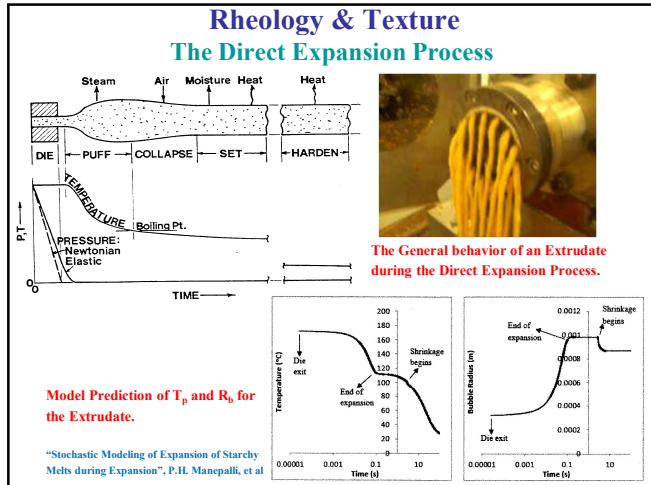
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Product Water Solubility



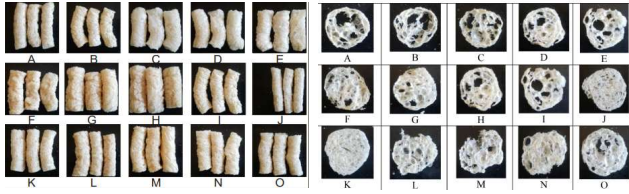
Increasing the SME reduces the MMW, therefore increases the *Water Solubility* (or reduces the *Water Stability*) of *Products*.

The two *Products* are clearly *not* the same! The *Bowl Life* of the *Extruded Cornflake* is significantly reduced.



Rheology & Texture

Process Interactions with Expansion



Key
 (A=100°C X₁, 15% X₂, 8% X₃), (B=140°C X₁, 15% X₂, 8% X₃), (C=100°C X₁, 25% X₂, 8% X₃), (D=140°C X₁, 25% X₂, 8% X₃) (E=100°C X₁, 15% X₂, 24% X₃), (F=140°C X₁, 15% X₂, 24% X₃), (G=100°C X₁, 25% X₂, 24% X₃), (H=140°C X₁, 25% X₂, 24% X₃), (I=86.5°C X₁, 20% X₂, 16% X₃), (J=153.6°C X₁, 20% X₂, 16% X₃), (K=120°C X₁, 11.6% X₂, 16% X₃) (L=120°C X₁, 28.4% X₂, 16% X₃), (M=120°C X₁, 20% X₂, 2.55% X₃) (N=120°C X₁, 20% X₂, 24.5% X₃) (O=120°C X₁, 20% X₂, 16% X₃), X₁= Barrel temperature, X₂= Feed moisture content, X₃= Amount of cowpea added to rice.

"Statistical Modeling and Optimization of Processing Conditions of TSE Extruded Rice-Legume Instant Breakfast Gruel", N. Danbaba, et al.
 Arid Zone Journal of Engineering, Technology and Environment, December, 2018; Vol. 14(4): 693-712.

"The Golden Rules of Extrusion Technology"

Golden Rule # 2

Energy Inputs

$$E_{\text{total}} = E_{\text{mechanical}} + E_{\text{convective}} + E_{\text{conductive}}$$

Total Energy
Input

Net Power
Input

Latent Energy
Input / Removal

Barrel Heat
Transfer

where

$$E_{\text{mechanical}} = f[\text{Rheology, Strain}]$$

$$E_{\text{convective}} = f[\text{Volatiles* Injection / Removal}] \quad (\text{Typically Steam})$$

$$E_{\text{conductive}} = f[\text{Barrel Temperature}]$$

Note : The Energy Inputs are **not** directly interchangeable!

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Direct Expansion of a Modified Starch
 (Prepared via Chemical Reaction in the Extruder)



Direct Expansion of a High Protein Formulation



Direct Expansion of Crumpet Flour